

# Lecture 17

## Dielectric Waveguides

Before we embark on the study of dielectric waveguides, we will revisit the transverse resonance again. The transverse resonance condition allows one to derive the guidance conditions for a dielectric waveguide easily without having to match the boundary conditions at the interface again: The boundary conditions are already used when deriving the Fresnel reflection coefficients, and hence they are embedded in these reflection coefficients. Much of the materials in this lecture can be found in [31, 38, 75].

### 17.1 Generalized Transverse Resonance Condition

The guidance conditions, the transverse resonance condition given previously, can also be derived for the more general case. The generalized transverse resonance condition is a powerful condition that can be used to derive the guidance condition of a mode in a layered medium.

To derive this condition, we first have to realize that a guided mode in a waveguide is due to the coherent or constructive interference of the waves. This implies that if a plane wave starts at position 1 (see Figure 17.1)<sup>1</sup> and is multiply reflected as shown, it will regain its original phase in the  $x$  direction at position 5. Since this mode progresses in the  $z$  direction, all these waves (also known as partial waves) are in phase in the  $z$  direction by the phase matching condition. Otherwise, the boundary conditions cannot be satisfied. That is, waves at 1 and 5 will gain the same phase in the  $z$  direction. But, for them to add coherently or interfere coherently in the  $x$  direction, the transverse phase at 5 must be the same as 1.

Assuming that the wave starts with amplitude 1 at position 1, it will gain a transverse phase of  $e^{-j\beta_{0x}t}$  when it reaches position 2. Upon reflection at  $x = x_2$ , at position 3, the wave becomes  $\tilde{R}_+ e^{-j\beta_{0x}t}$  where  $\tilde{R}_+$  is the generalized reflection coefficient at the right interface of Region 0. Finally, at position 5, it becomes  $\tilde{R}_- \tilde{R}_+ e^{-2j\beta_{0x}t}$  where  $\tilde{R}_-$  is the generalized reflection coefficient at the left interface of Region 0. For constructive interference to occur

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<sup>1</sup>The waveguide convention is to assume the direction of propagation to be  $z$ . Since we are analyzing a guided mode in a layered medium,  $z$  axis is as shown in this figure.

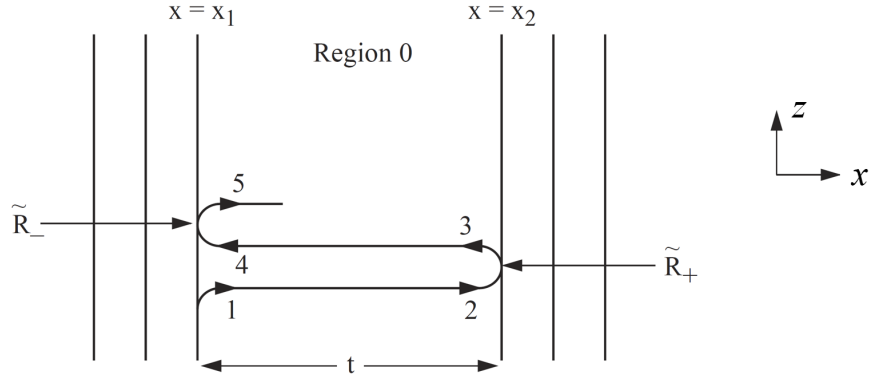


Figure 17.1: The transverse resonance condition for a layered medium. The phase of the wave at position 5 should be equal to the transverse phase at position 1.

or for the mode to exist, we require that

$$\tilde{R}_- \tilde{R}_+ e^{-2j\beta_{0x}t} = 1 \quad (17.1.1)$$

The above is the generalized transverse resonance condition for the guidance condition for a plane wave mode traveling in a layered medium.

In (17.1.1), a metallic wall has a reflection coefficient of 1 for a TM wave, hence if  $\tilde{R}_+$  is 1, Equation (17.1.1) becomes

$$1 - \tilde{R}_- e^{2-j\beta_{0x}t} = 0. \quad (17.1.2)$$

On the other hand, in (17.1.1), a metallic wall has a reflection coefficient of  $-1$ , for TE wave, and Equation (17.1.1) becomes

$$1 + \tilde{R}_- e^{2-j\beta_{0x}t} = 0. \quad (17.1.3)$$

## 17.2 Dielectric Waveguide

The most important dielectric waveguide of the modern world is the optical fiber, whose invention was credited to Charles Kao [91]. He was awarded the Nobel prize in 2009 [102]. However, the analysis of the optical fiber requires analysis in cylindrical coordinates and the use of special functions such as Bessel functions. In order to capture the essence of dielectric waveguides, one can study the slab dielectric waveguide, which shares many salient features with the optical fiber. This waveguide is also used as thin-film optical waveguides (see Figure 17.2). We start with analyzing the TE modes in this waveguide.

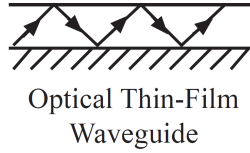


Figure 17.2: An optical thin-film waveguide is made by coating a thin dielectric film or sheet on a metallic surface. The wave is guided by total internal reflection at the top interface, and by metallic reflection at the bottom interface.

### 17.2.1 TE Case

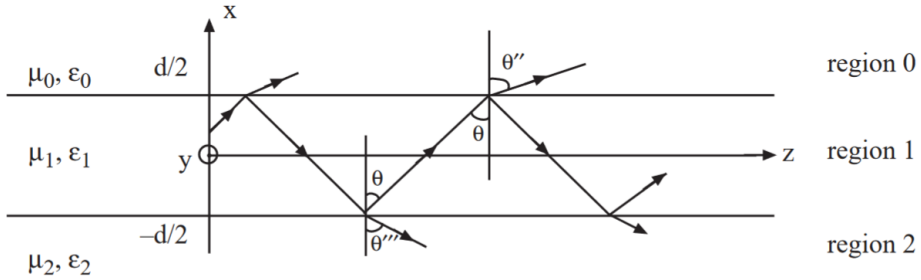


Figure 17.3: Schematic for the analysis of a guided mode in the dielectric waveguide. Total internal reflection occurs at the top and bottom interfaces. If the waves add coherently, the wave is guided along the dielectric slab.

We shall look at the application of the transverse resonance condition to a TE wave guided in a dielectric waveguide. Again, we assume the direction of propagation of the guided mode to be in the  $z$  direction in accordance to convention. Specializing the above equation to the dielectric waveguide shown in Figure 17.3, we have the guidance condition as

$$1 = R_{10}R_{12}e^{-2j\beta_{1x}d} \tag{17.2.1}$$

where  $d$  is the thickness of the dielectric slab. Guidance of a mode is due to total internal reflection, and hence, we expect Region 1 to be optically more dense (in terms of optical refractive indices)<sup>2</sup> than region 0 and 2.

To simplify the analysis further, we assume Region 2 to be the same as Region 0. The new guidance condition is then

$$1 = R_{10}^2 e^{-2j\beta_{1x}d} \tag{17.2.2}$$

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<sup>2</sup>Optically more dense means higher optical refractive index, or higher dielectric constant.

Also, we assume that  $\varepsilon_1 > \varepsilon_0$  so that total internal reflection occurs at both interfaces as the wave bounces around so that  $\beta_{0x} = -j\alpha_{0x}$ . Therefore, for TE polarization, the single-interface reflection coefficient is

$$R_{10} = \frac{\mu_0\beta_{1x} - \mu_1\beta_{0x}}{\mu_0\beta_{1x} + \mu_1\beta_{0x}} = \frac{\mu_0\beta_{1x} + j\mu_1\alpha_{0x}}{\mu_0\beta_{1x} - j\mu_1\alpha_{0x}} = e^{j\theta_{TE}} \quad (17.2.3)$$

where  $\theta_{TE}$  is the Goos-Hanschen shift for total internal reflection. It is given by

$$\theta_{TE} = 2 \tan^{-1} \left( \frac{\mu_1\alpha_{0x}}{\mu_0\beta_{1x}} \right) \quad (17.2.4)$$

The guidance condition for constructive interference according to (17.2.1) is such that

$$2\theta_{TE} - 2\beta_{1x}d = 2n\pi \quad (17.2.5)$$

From the above, dividing it by four, and taking its tangent, we get

$$\tan \left( \frac{\theta_{TE}}{2} \right) = \tan \left( \frac{n\pi}{2} + \frac{\beta_{1x}d}{2} \right) \quad (17.2.6)$$

or

$$\frac{\mu_1\alpha_{0x}}{\mu_0\beta_{1x}} = \tan \left( \frac{n\pi}{2} + \frac{\beta_{1x}d}{2} \right) \quad (17.2.7)$$

The above gives rise to

$$\mu_1\alpha_{0x} = \mu_0\beta_{1x} \tan \left( \frac{\beta_{1x}d}{2} \right), \quad n \text{ even} \quad (17.2.8)$$

$$-\mu_1\alpha_{0x} = \mu_0\beta_{1x} \cot \left( \frac{\beta_{1x}d}{2} \right), \quad n \text{ odd} \quad (17.2.9)$$

It can be shown that when  $n$  is even, the mode profile is even, whereas when  $n$  is odd, the mode profile is odd. The above can also be rewritten as

$$\frac{\mu_0}{\mu_1} \frac{\beta_{1x}d}{2} \tan \left( \frac{\beta_{1x}d}{2} \right) = \frac{\alpha_{0x}d}{2}, \quad \text{even modes} \quad (17.2.10)$$

$$-\frac{\mu_0}{\mu_1} \frac{\beta_{1x}d}{2} \cot \left( \frac{\beta_{1x}d}{2} \right) = \frac{\alpha_{0x}d}{2}, \quad \text{odd modes} \quad (17.2.11)$$

Using the fact that  $-\alpha_{0x}^2 = \beta_0^2 - \beta_z^2$ , and that  $\beta_{1x}^2 = \beta_1^2 - \beta_z^2$ , eliminating  $\beta_z$  from these two equations, one can show that

$$\alpha_{0x} = [\omega^2(\mu_1\varepsilon_1 - \mu_0\varepsilon_0) - \beta_{1x}^2]^{\frac{1}{2}} \quad (17.2.12)$$

and (17.2.10) and (17.2.11) become

$$\begin{aligned} \frac{\mu_0}{\mu_1} \frac{\beta_{1x} d}{2} \tan\left(\frac{\beta_{1x} d}{2}\right) &= \frac{\alpha_{0x} d}{2} \\ &= \sqrt{\omega^2(\mu_1 \epsilon_1 - \mu_0 \epsilon_0) \frac{d^2}{4} - \left(\frac{\beta_{1x} d}{2}\right)^2}, \quad \text{even modes} \end{aligned} \quad (17.2.13)$$

$$\begin{aligned} -\frac{\mu_0}{\mu_1} \frac{\beta_{1x} d}{2} \cot\left(\frac{\beta_{1x} d}{2}\right) &= \frac{\alpha_{0x} d}{2} \\ &= \sqrt{\omega^2(\mu_1 \epsilon_1 - \mu_0 \epsilon_0) \frac{d^2}{4} - \left(\frac{\beta_{1x} d}{2}\right)^2}, \quad \text{odd modes} \end{aligned} \quad (17.2.14)$$

We can solve the above graphically by plotting

$$y_1 = \frac{\mu_0}{\mu_1} \frac{\beta_{1x} d}{2} \tan\left(\frac{\beta_{1x} d}{2}\right) \quad \text{even modes} \quad (17.2.15)$$

$$y_2 = -\frac{\mu_0}{\mu_1} \frac{\beta_{1x} d}{2} \cot\left(\frac{\beta_{1x} d}{2}\right) \quad \text{odd modes} \quad (17.2.16)$$

$$y_3 = \left[ \omega^2(\mu_1 \epsilon_1 - \mu_0 \epsilon_0) \frac{d^2}{4} - \left(\frac{\beta_{1x} d}{2}\right)^2 \right]^{\frac{1}{2}} = \frac{\alpha_{0x} d}{2} \quad (17.2.17)$$

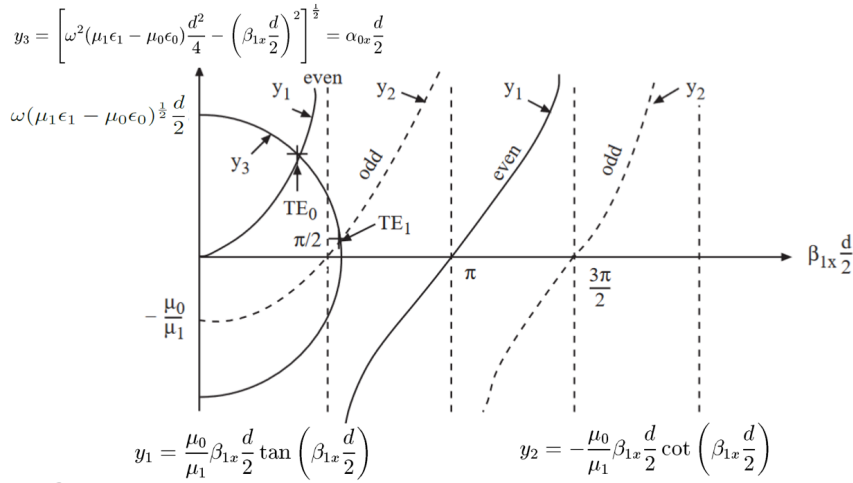


Figure 17.4: A way to solve (17.2.13) and (17.2.13) is via a graphical method. In this method, both the right-hand side and the left-hand side of the equations are plotted on the same plot. The solutions are the points of intersection of these plots.

In the above,  $y_3$  is the equation of a circle; the radius of the circle is given by

$$\omega(\mu_1\epsilon_1 - \mu_0\epsilon_0)^{\frac{1}{2}}\frac{d}{2}. \quad (17.2.18)$$

The solutions to (17.2.13) and (17.2.14) are given by the intersections of  $y_3$  with  $y_1$  and  $y_2$ . We note from (17.2.1) that the radius of the circle can be increased in three ways: (i) by increasing the frequency, (ii) by increasing the contrast  $\frac{\mu_1\epsilon_1}{\mu_0\epsilon_0}$ , and (iii) by increasing the thickness  $d$  of the slab.<sup>3</sup> The mode profiles of the first two modes are shown in Figure 17.5.

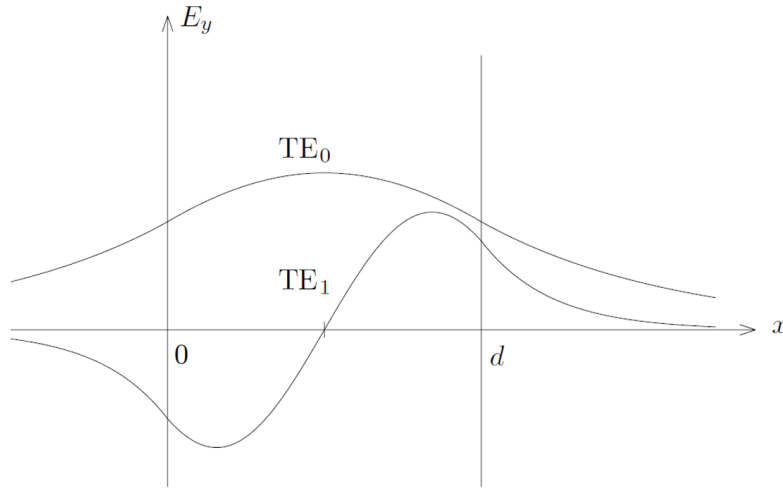


Figure 17.5: Mode profiles of the  $TE_0$  and  $TE_1$  modes of a dielectric slab waveguide (courtesy of J.A. Kong [31]).

When  $\beta_{0x} = -j\alpha_{0x}$ , the reflection coefficient for total internal reflection is

$$R_{10}^{TE} = \frac{\mu_0\beta_{1x} + j\mu_1\alpha_{0x}}{\mu_0\beta_{1x} - j\mu_1\alpha_{0x}} = \exp \left[ +2j \tan^{-1} \left( \frac{\mu_1\alpha_{0x}}{\mu_0\beta_{1x}} \right) \right] \quad (17.2.19)$$

and  $|R_{10}^{TE}| = 1$ . Hence, the wave is guided by total internal reflections.

**Cut-off occurs** when the total internal reflection ceases to occur, i.e. when the frequency decreases such that  $\alpha_{0x} = 0$ .

From Figure 17.4, we see that  $\alpha_{0x} = 0$  when

$$\omega(\mu_1\epsilon_1 - \mu_0\epsilon_0)^{\frac{1}{2}}\frac{d}{2} = \frac{m\pi}{2}, \quad m = 0, 1, 2, 3, \dots \quad (17.2.20)$$

<sup>3</sup>These features are also shared by the optical fiber.

or

$$\omega_{mc} = \frac{m\pi}{d(\mu_1\epsilon_1 - \mu_0\epsilon_0)^{\frac{1}{2}}}, \quad m = 0, 1, 2, 3, \dots \quad (17.2.21)$$

The mode that corresponds to the  $m$ -th cut-off frequency above is labeled the  $TE_m$  mode. Thus  $TE_0$  mode is the mode that has no cut-off or propagates at all frequencies. This is shown in Figure 17.6 where the TE mode profiles are similar since they are dual to each other. The boundary conditions at the dielectric interface is that the field and its normal derivative have to be continuous. The  $TE_0$  or  $TM_0$  mode can satisfy this boundary condition at all frequencies, but not the  $TE_1$  or  $TM_1$  mode. At the cut-off frequency, the field outside the slab has to become flat implying the  $\alpha_{0x} = 0$  implying no guidance.

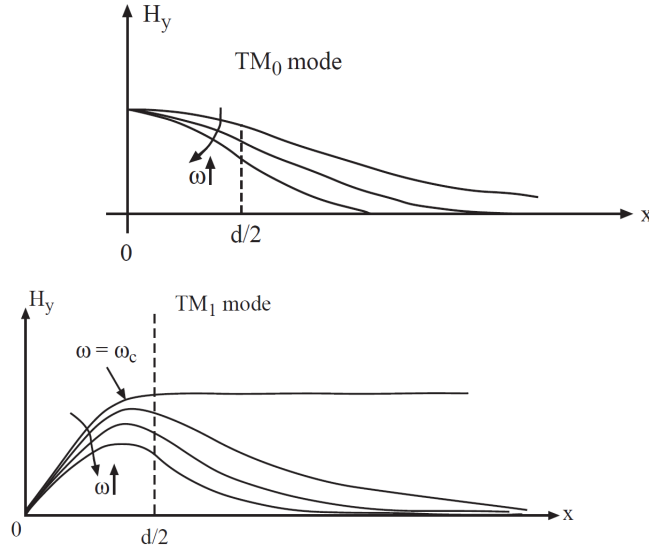


Figure 17.6: The TE modes are dual to the TM modes and have similar mode profiles.

At cut-off,  $\alpha_{0x} = 0$ , and from the dispersion relation that  $\alpha_{0x}^2 = \beta_z^2 - \beta_0^2$ ,

$$\beta_z = \omega\sqrt{\mu_0\epsilon_0},$$

for all the modes. Hence, both the group and the phase velocities are that of the outer region. This is because when  $\alpha_{0x} = 0$ , the wave is not evanescent outside, and most of the energy of the mode is carried by the exterior field.

When  $\omega \rightarrow \infty$ , the radius of the circle in the plot of  $y_3$  becomes increasingly larger. As seen from Figure 17.4, the solution for  $\beta_{1x} \rightarrow \frac{n\pi}{d}$  for all the modes. From the dispersion relation for Region 1,

$$\beta_z = \sqrt{\omega^2\mu_1\epsilon_1 - \beta_{1x}^2} \approx \omega\sqrt{\mu_1\epsilon_1}, \quad \omega \rightarrow \infty \quad (17.2.22)$$

Hence the group and phase velocities approach that of the dielectric slab. This is because when  $\omega \rightarrow \infty$ ,  $\alpha_{0x} \rightarrow \infty$ , implying that the fields are trapped or confined in the slab and propagating within it. Because of this, the dispersion diagram of the different modes appear as shown in Figure 17.7. In this figure,<sup>4</sup>  $k_{c1}$ ,  $k_{c2}$ , and  $k_{c3}$  are the cut-off wave number or frequency of the first three modes. Close to cut-off, the field is traveling mostly outside the waveguide, and  $k_z \approx \omega\sqrt{\mu_0\epsilon_0}$ , and both the phase and group velocities approach that of the outer medium as shown in the figure. When the frequency increases, the mode is tightly confined in the dielectric slab, and  $k_z \approx \omega\sqrt{\mu_1\epsilon_1}$ . Both the phase and group velocities approach that of Region 1 as shown.

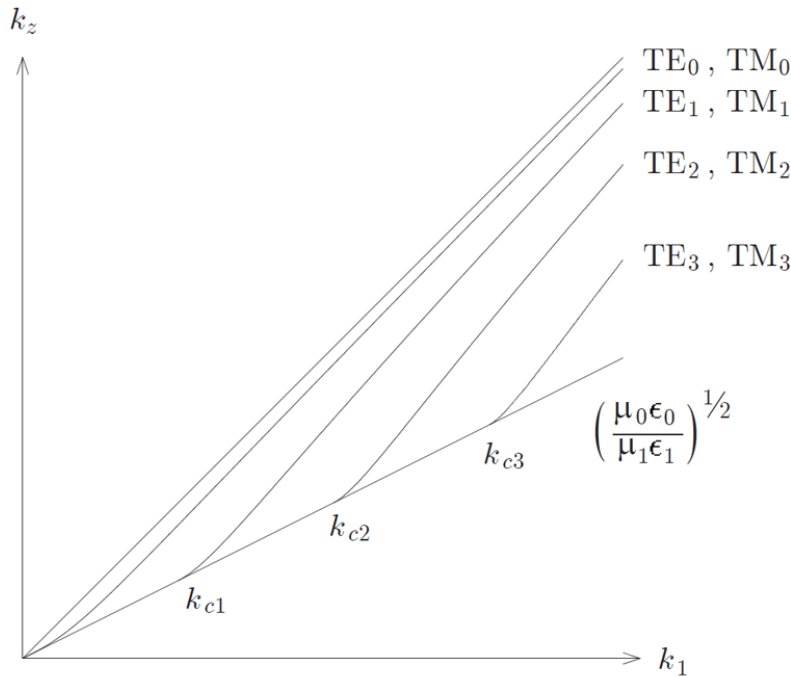


Figure 17.7: Here, we have  $k_z$  versus  $k_1$  plot for dielectric slab waveguide. Near its cut-off, the energy of the mode is in the outer region, and hence, its group velocity is close to that of the outer region. At high frequencies, the mode is tightly bound to the slab, and its group velocity approaches that of the dielectric slab (courtesy of J.A. Kong [31]).

## 17.2.2 TM Case

For the TM case, a similar guidance condition analogous to (17.2.1) can be derived but with the understanding that the reflection coefficients in (17.2.1) are now TM reflection coefficients.

<sup>4</sup>Please note again that in this course, we will use  $\beta$  and  $k$  interchangeably for wavenumbers.



Similar derivations show that the above guidance condition, for  $\epsilon_2 = \epsilon_0$ ,  $\mu_2 = \mu_0$ , reduces to

$$\frac{\epsilon_0}{\epsilon_1} \beta_{1x} \frac{d}{2} \tan \beta_{1x} \frac{d}{2} = \sqrt{\omega^2 (\mu_1 \epsilon_1 - \mu_0 \epsilon_0) \frac{d^2}{4} - \left( \beta_{1x} \frac{d}{2} \right)^2}, \quad \text{even modes} \quad (17.2.23)$$

$$-\frac{\epsilon_0}{\epsilon_1} \beta_{1x} \frac{d}{2} \cot \beta_{1x} \frac{d}{2} = \sqrt{\omega^2 (\mu_1 \epsilon_1 - \mu_0 \epsilon_0) \frac{d^2}{4} - \left( \beta_{1x} \frac{d}{2} \right)^2}, \quad \text{odd modes} \quad (17.2.24)$$

Note that for equation (17.2.1), when we have two parallel metallic plates,  $R^{TM} = 1$ , and  $R^{TE} = -1$ , and the guidance condition becomes

$$1 = e^{-2j\beta_{1x}d} \Rightarrow \beta_{1x} = \frac{m\pi}{d}, \quad m = 0, 1, 2, \dots, \quad (17.2.25)$$

### 17.2.3 A Note on Cut-Off of Dielectric Waveguides

The concept of cut-off in dielectric waveguides is quite different from that of hollow waveguides that we shall learn next. A mode is guided in a dielectric waveguide if the wave is trapped inside, in this case, the dielectric slab. The trapping is due to the total internal reflections at the top and the bottom interface of the waveguide. When total internal reflection ceases to occur at any of the two interfaces, the wave is not guided or trapped inside the dielectric slab anymore. This happens when  $\alpha_{ix} = 0$  where  $i$  can indicate the top-most or the bottom-most region. In other words, the wave ceases to be evanescent in Region  $i$ .

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26 décembre 1820, 10 juin 1822, 22 décembre 1823, 12 septembre et 21 novembre 1825. Bachelier, 1825.

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